

## Fuel cell comprising a magnetic cathode with static pumping

### Background of the invention

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The invention relates to a fuel cell generating electric power from oxygen and hydronium ions, and comprising an anode, a magnetic cathode comprising an active layer, a proton electrolyte between the anode and the cathode, and a network of permanent magnets having magnetic axes perpendicular to the interface between the electrolyte and the active layer, the magnets comprising a first pole and a second pole.

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### State of the art

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Fuel cells are constituted by an anode and a cathode separated by a liquid or polymer electrolyte. For certain applications, in particular power supply of portable electronic devices, one of the fuels is the oxygen of the air. The performances of such a system are limited essentially by the cathode and in particular by the quantity of oxygen accessible at the level of the catalyzer. The use of a conventional pumping system increasing the oxygen flow at the level of the cathode is costly in energy, the associated performance increase then being compensated by the energy consumed by the pumping system.

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It would be interesting to make the fuel cell operate by using the oxygen present in the ambient air to the maximum without a mechanical pumping system. A solution called "static pumping" has been proposed, using the paramagnetic properties of oxygen. Static pumping is based on the force exerted on a paramagnetic object by a magnetic field in which it is situated. In a magnetic

field this force attracts the paramagnetic object in the direction in which the absolute value of the magnetic field increases.

5 The article "Magnetic Promotion of Oxygen Reduction Reaction with Pt Catalyst in Sulfuric Acid Solutions" by N.I. WAKAYAMA *et Al.* proposed improving the operation of a fuel cell by static pumping (Jpn. J. Appl. Phys. Vol. 40 (2001) pp. L269-L271) by incorporating a powder of small magnetic particles in an active layer between a membrane and a diffusion electrode. However, this solution has a very small effect, because the magnetic particles are distributed in random  
10 manner over the whole thickness of the active layer.

The document JP 2002/198,057 describes a fuel cell comprising permanent magnets dispersed in one of the electrodes of a fuel cell. The magnets can be arranged in a network and the orientations of the permanent magnets are  
15 uniform and parallel to a line connecting the electrodes.

Consequently, in the two above-mentioned documents, the resulting magnetic force is reduced in the points of the space where the magnetic fields of several particles or magnets are opposed. The oxygen is not attracted by the magnetic  
20 forces to penetrate into the whole volume of the active layer. The operation of the active layer is then improved on the surface only, whereas the operation within the volume remains weakened.

Another drawback of small magnetic particles is the large corrosion of the  
25 magnetic material in an acid or even alkaline medium depending on the type of cell envisaged.

## **Object of the invention**

The object of the invention is to remedy these shortcomings and in particular to increase the quantity of oxygen accessible at the level of the whole of the catalyzer of the active cathodic layer.

According to the invention, this object is achieved by the accompanying claims and more particularly by the fact that the first and second poles of the magnets of the network are respectively arranged in an active layer and in the electrolyte.

## **Brief description of the drawings**

Other advantages and features will become more clearly apparent from the following description of particular embodiments of the invention given as non-restrictive examples only and represented in the accompanying drawings, in which:

Figure 1 is a representation of an embodiment of a fuel cell according to the invention.

Figure 2 illustrates the variations of the magnetic force inside the cell.

Figures 3 and 4 are cross-sectional views along the vertical axis 8 of different embodiments of the cell according to figure 1.

Figure 5 schematically represents the symmetry of another particular embodiment of a network of permanent magnets.

## **Description of particular embodiments.**

Figure 1 represents a fuel cell comprising an anode A, a proton electrolyte 1 and a magnetic cathode comprising an active layer 2, a porous electric current collector plate 5 and a diffusion layer 6. The oxygen arriving from the right passes through the collector plate 5 and the diffusion layer 6 of the cathode and enters the active layer. The hydrogen comes in the form of hydronium ions (usually called  $H^+$ ), borne by a compound able to be a hydrogen vector (alcohol, sugar, nitrogenated compound, etc...).

To increase the diffusion of the oxygen entering the active layer 2, the cathode comprises a network 3 of permanent magnets 4 having magnetic axes perpendicular to the interface between the electrolyte and the active layer.

In a preferred embodiment, the centers of the magnets 4 of the network 3 of permanent magnets are arranged with a two-dimensional distribution. In figure 1, this two-dimensional distribution is localized in the plane parallel to the interface between the electrolyte 1 and the active layer 2. The magnets 4 are preferably magnetized along the axis z perpendicular to the plane of the two-dimensional distribution so that all the north polarity poles N are in one plane and all the south polarity poles S are in a parallel plane. In this way, first poles S of the magnets 4 of the network 3 are arranged in a first plane parallel to the interface between the electrolyte 1 and the active layer 2 and second poles N of the magnets 4 of the network 3 are arranged in a second plane parallel to the interface between the electrolyte 1 and the active layer 2.

In a preferred embodiment, the permanent magnets 4 are semi-surrounded by the active layer 2 so that all the poles (S) of the same polarity are surrounded by the active layer 2, all the poles of opposite polarity (N) being surrounded by the electrolyte 1. In this way, the first and second planes are respectively arranged in the active layer 2 and in the electrolyte 1. In the embodiment represented in

figure 1, the interface between the electrolyte 1 and the active layer 2 is arranged substantially at equal distance from the first and second planes. The permanent magnets 4 preferably have identical shapes and identical spatial orientations, as represented in figure 1.

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In the embodiment represented in figure 1, the interface between the electrolyte and the active layer is situated on a vertical axis 8 and the magnets are magnetized along a horizontal axis  $z$ . The magnets then create a magnetic field, the absolute value whereof is maximal on the vertical axis 8. A magnetic force  $F(z)$  attracts the oxygen to the vertical axis 8.

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In figure 2, the magnetic force  $F(z)$  is illustrated as a function of the coordinate on the horizontal axis  $z$ . The force  $F(z)$  increases when the vertical axis 8 is approached and changes sign precisely on the vertical axis 8, corresponding to a change of direction of the force. On the left part of the axis 8, the oxygen is then attracted to the right, whereas on the right part of the axis 8, the oxygen is then attracted to the left.

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The electrochemical reaction with the oxygen takes place in the entire active layer 2. This layer therefore has to be located in the region where the oxygen concentration is at the maximum. The oxygen coming from the diffusion zone 6 is attracted into the whole volume of the active layer by the magnets. On the other hand, in the electrolyte, the oxygen is repelled towards the active layer so that the oxygen concentration in the electrolyte is reduced. Insertion of the magnets partially in the active layer and partially in the electrolyte is optimized by the distribution of the magnets 50% in the active layer and 50% in the electrolyte.

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With reference to figure 3, the network of permanent magnets can be formed by cylindrical magnets 4 arranged in a two-dimensional distribution of a periodic network 10.

5 As represented in figure 4, the cell can comprise a support network 11 comprising apertures 12 wherein the magnets 4 can be arranged. The support comprises passages 13 for the ions, in particular the hydronium ions coming from the electrolyte, between the magnets. The passages 13 are therefore triple point zones where the hydronium ion  $H^+$ , oxygen  $O_2$  and electron elements are  
10 in presence, which gives rise to the electrochemical reaction. The material of the support network 11 can be a non-magnetic material. The support network can be fixed onto the electrolyte 1 or arranged at the interface between the electrolyte 1 and the active layer 2.

15 The performance of this improved oxygen diffusion system by a network 3 of magnets 4 depends on the variation of several parameters: the magnetization, the geometry and number of magnets 4, the thickness of the cathode and the geometric distribution of the magnets 4 and of the passages 13 for the hydronium ions. In this way, with a flat periodic distribution of the centers of the  
20 masses of the magnets 4, as in figure 3, a uniform improvement of the gas diffusion in the catalyzer is obtained. Other flat geometries, for example triangular or fractal, can also be envisaged.

25 As represented in figure 5, a distribution of the apertures 12 for placing the magnets 4 and of the passages 13 in the support network 11 can constitute a fractal structure, represented by triangles of different dimensions, a relatively large triangle being surrounded by smaller triangles. The centers of the triangles of figure 5 represent the centers of the magnets. The individual shape of the magnets themselves is not necessarily triangular.

In order to prevent corrosion of the magnets 4 in the electrolyte 1 (acid or alkaline), the magnets 4 can be treated against corrosion or comprise anti-corrosive coatings (in figure 1, one of the magnets is represented with an anti-corrosive coating 14). The anti-corrosion treatment depends on the nature of the electrolyte 1. The material of the coating is typically platinum or gold.

The network 3 of permanent magnets 4 can comprise magnets 4 made of ferromagnetic material. For example, the permanent magnets 4 can be made from materials forming part of the SmCo, AlNiCo, NdFeB or Ferrite families. However, any magnetic metals and alloys are envisageable.

The best performances are obtained if the magnets 4 are very close to the oxygen, i.e. on the cathode side. However, an optimum oxygen diffusion throughout the cathode is obtained with the embodiment of figure 1 wherein the centers of the magnets 4 are located on the interface between the active layer 2 of the cathode and the electrolyte 1. The magnetic forces increase quickly when the distance between the magnets 4 and the oxygen decreases. In this way, the network 3 of magnets 4 operates as a filter of the oxygen in the air, privileging oxygen over the other gases present in the air.

The permanent magnets 4 constitute an ideal magnetic field source, operating alone, without an additional external energy input.

The invention is more particularly suited to fabrication of mini-fuel cells. The network 3 of magnets 4 enables a sufficient magnetic force to be produced at a distance of a few millimeters from the active layer 2. This enables a reduction of the overpotential of the oxygen reduction reaction to be obtained, as indicated by the following example: in the case of a fuel cell comprising a solid polymer

electrolyte with a cathode with a thickness of about  $250\mu\text{m}$  and a resulting magnetic field of the magnets of  $10^{-6}$  teslas, a decrease of the diffusion overpotential of about 10% to 20% can be forecast.